# EXPERIMENTAL RESEARCH ON THE KNIFE BLADES USED TO CUTTING AND SHREDDING FIBROUS FODDER

# CERCETĂRI EXPERIMENTALE ASUPRA ORGANELOR DE TĂIERE-MĂRUNŢIRE A FURAJELOR FIBROASE

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#### **ABSTRACT**

In the process of harvesting fibrous fodder an important and negligible requirement is the appropriate shredding of the fiber feed directly or indirectly into the composition of animal feed, whether it be fresh fodder, high moisture or fodder feed or even dried. The degree of comminution of feeding stuffs decisively influences the speed of assimilation by animals of the administered feed, implicitly their weight gain, the profitability of the respective cattle farm and not only. In the paper are presented the possibilities of technically obtaining a finest shredding of fibrous fodder, especially by using multirow knives in the feed channel of self-loading hay trailer. However, these technical solutions also have certain disadvantages in the daily operation of such machines.

#### **REZUMAT**

În procesul de recoltare a furajelor fibroase o cerință importantă și de loc de neglijat este mărunțirea corespunzătoare a furajelor fibroase care intră direct sau indirect în componența hranei animalelor, indiferent dacă este vorba de furaje fibroase proaspete, cu un grad de umiditate ridicat sau despre furaje vestejite sau chiar uscate. Gradul de mărunțire a furajelor influențează în mod hotărâtor viteza de asimilare de către animale a nutrețului administrat, implicit sporul în greutate al acestora, rentabilitatea de funcționare a fermei respective de bovine și nu numai. În lucrare se prezintă posibilitățile de a obține tehnic o mărunțire cât mai bună a furajelor fibroase, cu precădere prin utilizarea a cuțitelor multiple așezate pe mai multe rânduri în canalul de alimentare ale remorcilor autoîncărcătoare fân. Aceste soluții tehnice însă prezintă și anumite dezavantaje în exploatare de zi cu zi ale utilajelor de acest gen.

## INTRODUCTION

In order to counteract all these shortcomings presented above, we carried out some theoretical research, resulting in a universal knife profile, which has the advantage of general usability.

Its profile is thus conceived from the design stage to meet the requirements of cutting - shredding of all types of green fodder feed used in animal feed in zootechnics, regardless of their degree of humidity.

In the experimental researches we performed a series of cutting - shredding tests on different types and kinds of fibrous feeds in order to establish the correctness regarding the results of the experimental research and the actual shape of the knife obtained from the researches.

For this purpose, we designed and executed a cutting bench at the laboratory, where we used different forms of knives to determine the specific energy needed to cut different types of fibrous feed (*Caba I., 2006; Babinszky L., Halas V., 2019*).

#### **MATERIALS AND METHODS**

In order to carry out experimental laboratory tests to ascertain the usefulness and viability of the projected knife profile, it was necessary to design and execute a test stand where successive, repeated cuts with different shapes and sharpening angles could be performed, where the section of the test samples fodder feed remained constant and measurable at all times (*Ciocârdia C., 1999; Dănilă I., 1981; Neculăiasa V., Dănilă I., 1995*). The actual operation scheme is shown in Figure 1.

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Another requirement was ease, simplicity and last but not least the safety of clamping of different shapes of their edges. The basic element of the experimental laboratory tests was the Charpy pendulum (*Dutton A. and Mines R., 2002; Truşculescu M., 2016*), for which we designed and built a special support device for easy gripping of the knives and samples. This support allowed the knives to snap and loosen easily and ensured that they were hardened during the laboratory experiment. The clamping-fastening device of the knife is made up of a metal plate identical in shape to the pendulum profile. Stiffening of this plate (the knife holder) to the pendulum profile was accomplished by the application of four fastening heels welded to the surface of the plate. On the surface of the disc, I have reinforced with electric arc welding four clamping clamps, which serve to stiffen the cutting and grinding blade during the measurements, but also allow for a slight change of the clamp.

Balancing the accessories applied to the surface of the pendulum profile was done with great care, while recording these values. The weight of the initial hammer arm of 2074 g was reached after the knife fastening device was mounted at 2530 g, but the balancing was so carefully chosen that it did not significantly change the center of gravity of the knife.

Another urgent necessity has also been to provide a certain distance between the knife and the hammer, failure to meet this requirement, and the removal of the detached part by cutting from the length of the specimen automatically led to the locking of the cutting knife in the feed material used as the test samples. In order to achieve a proper grip of the feed material specimen and to ensure a constant cutting section throughout the measurements, we designed and made a simple clamping vice, with three rigid walls and a fourth movable. Thus, we ensured a cross section of the constant and measurable specimen. The vise movable wall was operated with a press screw, and the vise supply was possible by completely detaching the movable wall and its support bracket into stiffening screws.

The drawings of the Charpy hammer pendulum are shown in Figure 2, which allows us to easily determine the specific energy consumed in the cutting of the fibrous feed specimen and the technical data related to this device used in the experimental determinations made in the laboratory are as follows:

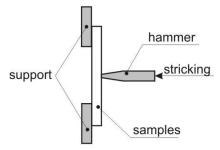


Fig. 1 - The principle of the test

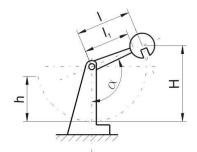


Fig. 2 - Scheme of Charpy hammer operation

## where:

- l the distance from the axis of rotation the suspension at the cutting center of the knife blades, in this case l = 0.380 m;
- $l_{I}$  distance from rotation axis suspension at the center of gravity, having the following value  $l_{I}$  = 0.335 m;
  - d angle of hammer launch, in the present case  $\alpha = 130^{\circ}$ ;
- $\beta$  the angle of maximum hammer position after cutting of the specimen, read on the graduated screen of the appliance;
  - *H* the hammer launch height;

h - the height at which the hammer is lifted after cutting the specimen

In the case mentioned above for the equilibrium position of the pendulum hammer, the condition is that:

$$Gl \neq G_1 l_1 \tag{1}$$

where:  $G_1$  - the weight of the hammer;

*G* - the weight of the hammer reduced in the percussion center.

The energy consumed when cutting a fiber feed specimen is determined by calculating the difference between potential potentials of the Charpy pendulum hammer in the initial and final position.

By calculating the heights H and h we obtain:

$$H = I_1 + I_1 \sin(\alpha - 90^0) = I_1 (1 - \cos \alpha)$$
 (2)

$$h = I_1 - I_1 \cos \beta = I_1 (1 - \cos \beta) \tag{3}$$

of these two relationships, the value of the energy W consumed at the cutting of the fibrous feed specimen results:

$$W = G_1 I_1 (\cos \beta - \cos \alpha) \tag{4}$$

With this cut-off energy calculated with the above relationship, we can easily determine the value of the specific energy used to cut the surface unit:

$$W_{\rm S} = W/S_{\rm O} \tag{5}$$

where:  $S_0$  - surface area of the fibrous feed material specimen.

Knowing the angular values, the hammer weight and the length from the axis of rotation to the cutting center (values determined in the laboratory experiments), we can obtain the specific energy and cutting energy values for each cut. These calculated and tilted values can also be graphical.

The working procedure in the Charpy hammer-pendulum experiments and the fibrous feed samples were practically carried out as follows:

- 1. place the indicator needle at zero on the dial with the hammer left in the static equilibrium position;
- 2. raise the hammer and fasten it to the heel, place the knife in the holder;
- 3. place the test samples of the fibrous feed material on the support of the apparatus so that one end of it is locked in the vise and the other end is free, measure the dimensions of the samples by means of a caliper, make adjustments with the central screw if it is applicable;
- 4. the fall occurs;
- 5. after cutting the samples, stop the hammer and read the values indicated by the needle from the dial:
- 6. collect the comminuted feed material by repeated cuts into the capsules to determine the moisture content of the samples used.

These tests have been repeatedly carried out for cutters having the cutting angle between  $0^{\circ}$ ,  $20^{\circ}$ ,  $25^{\circ}$  and  $30^{\circ}$  and the cutting edge angle of  $20^{\circ}$ . The sliding cutting angle represents the angular cutting tangent and had the values k = 0.57 for  $\alpha$  =  $30^{\circ}$ ; k = 0.46 for  $\alpha$  =  $25^{\circ}$  and k = 0.36 for  $\alpha$  =  $20^{\circ}$  (*Krasznicsenko A., 1965; Letoşnev M., 1969*).

The laboratory experiment was performed on samples of fibrous feed material, which is used mainly in livestock breeding for livestock feed.  $S_o$  we used lucerne, in the two versions available at the moment, cornstalk, sunflower and freshly harvested lolium pasture grass and we also made some attempts on dried wheat straw. After each cut, we collected the detached material and proceeded to determine the moisture content of the specimen (*Nosov V., 1988; Szendro P., 2000; Bellus Z., Fenyvesi L., 2016*).

The fibrous feed material, detached by cutting the knife, was placed in crucibles, weighed, dried in the oven, and then weighed again (*Zaman A., Sagar M., 2018*). The data thus obtained were tabulated. Also in these tables are the values indicated by the needle on the graduated dial, whenever cuts are made. Several determinations were made with each knife profile, precisely to ensure accuracy in the processing and interpretation of the results obtained from experimental laboratory tests.

#### **RESULTS**

Following experimental laboratory determinations carried out using the Charpy hammer pendulum simulating the actual cutting of the fibrous feeds made by the grinding knives of the furrow-gathering

Table 2

machines during its exploitation, we find that an almost perfect simulation of the phenomena what is happening in reality.

Here, I refer to the grinding process - cutting which is made by knives, existing in a larger or smaller number, inside the feed channel, constructive part of self-loading hay trailers, cutting knives of different types, in function the type of feed, the way of feeding the feed furnace at the moment of penetration into the feed channel, its degree of humidity, the way of laying the knives in the groove, the profile of their cutting line, the angle of sharpening, the material used to make the knife, the frequency sharpening, s.o. Keeping the sharpening angle at 20°, we try blades with different angles of bend in order to determine the specific energy when cutting (*Csulak A. and Stoica A., 1968; Gainov N.S., 1985*).

These experimental laboratory tests should indicate the ideal profile of a knife that if we have correctly calculated it should be similar to the one we obtained from the calculations. The fodder materials used for the test specimens are as follows: freshly harvested lucerne; semy dry lucerne; lolium; dry wheat straw; corn stalk; sunflower stem. The results obtained are shown in the tables as follows:

Table 1

Cut	Cutting the fresh lucerne samples. Cutting angle kni $0^{0}$ , sharpening angle $20^{0}$					Cutting				utting angle
		0º, sharp	pening an	gle 20 <sup>0</sup>			knife 0°,	sharpeni	ng angle 2	25°
Nr.	Test-bar	Angle	Energy	Specific		Test-bar	Angle	Energy	Specific	
crt.	size	indicator	needed to	energy to	Observation	size	indicator	needed to	energy to	Observation
Cit.	(mm/mm)	(°)	cut (J)	cut (J/cm²)		(mm/mm)	(°)	cut (J)	cut (J/cm²)	
1	27*27	117	1.57	0.58	Tim of the otens	27*27	112	2.23	0.82	Tin of the estates
2	27*27	117	1.57	0.58	Tip of the stem with leaves	27*27	112	2.23	0.82	Tip of the stem with leaves
3	27*27	116	1.70	0.63	with leaves	27*27	111	2.36	0.87	with leaves
4	27*27	114	1.96	0.73	Dada and	27*27	110	2.50	0.93	De de en d
5	27*27	112	2.23	0.82	Rods and	27*27	110	2.50	0.93	Rods and
6	27*27	113	2.09	0.78	leaves	27*27	109	2.64	0.98	leaves
7	27*27	113	2.09	0.78	5	27*27	105	3.19	1.18	5
8	27*27	109	2.64	0.98	Rods at the	27*27	103	3.47	1.29	Rods at the
9	27*27	109	2.64	0.98	harvesting level	27*27	101	3.76	1.31	harvesting level
I.					Table 3			1	ı	Table 4
Cutti	ing the fre	sh lucern	e samples	. Cutting	angle knife	Cutting	g the lucer	ne lucern	e samples	s. Cutting
		<sup>0</sup> , angle o	f sharpen	ina 30°			gle knife (			
	Test-	, ,	<u> </u>	1				, ,		
NI.	bar	Angle	Energy	Specific		Test-bar	Angle	Energy	Specific	Ohaan
Nr.	size	indicator	needed	energy to cut	Obser-	size	indicator	needed	energy	Obser-
crt.	(mm	(°)	to cut (J)	(J/cm <sup>2</sup> )	vation	(mm /mm)	(°)	to cut (J)	to cut (J/cm <sup>2</sup> )	vation
	/mm)			(3/6111)		/111111)			(3/6111)	
1	27*27	104	3.33	1.23	Tip of the	27*27	105	3.19	1.18	Tip with
2	27*27	103	3.47	1.29	stem with	27*27	104	3.33	1.23	leaves
3	27*27	103	3.47	1.29	leaves	27*27	104	3.33	1.23	.00.00
4	27*27	99	4.04	1.50	Rods and	27*27	101	3.76	1.39	Rods and
5	27*27	97	4.33	1.60	leaves	27*27	101	3.76	1.39	leaves
6	27*27	95	4.62	1.71		27*27	100	3.90	1.44	
7	27*27	94	4.62	1.76	Rods at	27*27	98	4.19	1.55	Rods at the
8	27*27	94	4.62	1.76	the	27*27	98	4.19	1.55	harvesting
9	27*27	92	5.05	1.87	harvesting	27*27	96	4.19	1.66	level
					Table 5					Table 6
Cut	ting the se	my dry lu	corno can	anlos Cui	ting angle	Cuttino	the semu	dry lucor	no samali	es. Cutting
Cuti		ife 0º, sha			ung angle		ngle knife 0			
Nr.	Test-bar	Angle	Energy	Specific		Test-bar	Angle	Energy	Specific	y 30
crt.	size	indicator	needed	energy to	Obser-	size	indicator	needed	energy to	Obser-
Ort.	(mm	(°)	to cut (J)	cut (J/cm <sup>2</sup> )	vation	(mm	(°)	to cut (J)	cut	vation
	/mm)	( )	10 001 (0)	out (o/orri )	Vauori	/mm)	()	10 001 (0)	(J/cm <sup>2</sup> )	Valori
1	27*27	100	3.90	1.44	† <u> </u>	27*27	94	4.76	1.76	Tip with
2	27*27	98	4.19	1.55	Tip with	27*27	93	4.90	1.82	leaves
3	27*27	99	4.04	1.50	leaves -	27*27	93	4.90	1.82	
4	27*27	95	4.62	1.71	Strains	27*27	92	5.05	1.87	Otracia in
5	27*27	95	4.62	1.71	with	27*27	90	5.34	1.98	Strains with
6	27*27	93	4.90	1.82	leaves	27*27	90	5.34	1.98	leaves
7	27*27	92	5.05	1.87	Rods at	27*27	88	5.63	2.09	Rods at the
8	27*27	90	5.34	1.98	the	27*27	88	5.63	2.09	harvesting
L					1					

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9	27*27	89	5.49	2.03	harvesting	27*27	88	5.63	2.09	level
					level					

					Table 7					Table 8
Cu	tting the v	heat strav	v samples	s. Cutting ar	ngle knife	Cutting	the wheat	t straw sa	mples. Cu	tting angle
		0º, sharp	ening an	gle 20 <sup>0</sup>			knife 0°,	sharpenii	ng angle 2	5 <sup>0</sup>
Nr.	Test-bar	Angle	Energy	Specific	Obser-	Test-bar	Angle	Energy	Specific	Obser-
crt.	size	indicator	needed	energy to	vation	size	indicator	needed	energy to	vation
	(mm	(°)	to cut (J)	cut (J/cm²)		(mm	(°)	to cut (J)	cut	
	/mm)					/mm)			(J/cm <sup>2</sup> )	
1	27*27	90	5.34	1.98	Rods	27*27	88	5.63	2.09	Rods
2	27*27	89	5.49	2.03		27*27	86	5.92	2.19	
3	27*27	89	5.49	2.03		27*27	86	5.92	2.19	
4	27*27	87	5.78	2.14	Rods	27*27	83	6.36	2.35	Rods
5	27*27	85	6.07	2.25		27*27	82	6.50	2.41	
6	27*27	86	5.92	2.19		27*27	80	6.79	2.51	
7	27*27	84	6.21	2.30	Rods	27*27	79	6.93	2.57	Rods
8	27*27	84	6.21	2.30	1	27*27	79	6.93	2.57	
9	27*27	82	6.50	2.41		27*27	79	6.93	2.57	
					Table 9					Table 10
Cu	tting the w	heat strav	v samples	s. Cutting ar	ngle knife	Cutting	the Ioliun	n samples	. Cutting a	ngle knife
		0°, angle	of sharper	ning 30 $^{\circ}$			0°, sh	arpening	angle 20 <sup>0</sup>	
Nr.	Test-bar	Angle	Energy	Specific	Obser-	Test-bar	Angle	Energy	Specific	Obser-
crt.	size	indicator	needed	energy to	vation	size	indicator	needed	energy to	vation
	(mm	(°)	to cut (J)	cut (J/cm²)		(mm	(°)	to cut (J)	cut	
	/mm)					/mm)			(J/cm <sup>2</sup> )	
1	27*27	83	6.36	2.35	Rods	27*27	98	4.19	1.55	Strains and
2	27*27	82	6.50	2.41		27*27	97	4.33	1.60	leaves
3	27*27	83	6.36	2.35	1	27*27	96	4.47	1.66	
4	27*27	81	6.64	2.46	Rods	27*27	95	4.62	1.71	Strains and
5	27*27	80	6.69	2.51	] [	27*27	93	4.90	1.82	leaves
6	27*27	79	6.93	2.57	] [	27*27	91	5.20	1.92	
7	27*27	79	6.93	2.57	Rods	27*27	89	5.49	2.03	Strains and
8	27*27	75	7.50	2.78	1	27*27	89	5.49	2.03	leaves
9	27*27	75	7.50	2.78	] [	27*27	88	5.63	2.09	

0	21 21	75	7.50	2.70		21 21	69	5.49	2.03	leaves
9	27*27	75	7.50	2.78		27*27	88	5.63	2.09	
•								•		
					Table 11					Table 12
С	utting the	lolium sai	mples. Cu	tting angle l	knife 0°,	Cutting to	he Iolium	samples.	Cutting an	gle knife $0^{\circ}$ ,
		sharpe	ning angl	e 25 <sup>0</sup>			angle	of sharpe	ening 30 <sup>0</sup>	
Nr.	Test-bar	Angle	Energy	Specific	Obser-	Test-bar	Angle	Energy	Specific	
crt.	size	indicator	needed to	energy to cut	vation	size	indicator	needed to	energy to	Obser-vation
CIT.	(mm/mm)	(°)	cut (J)	(J/cm <sup>2</sup> )	valion	(mm/mm)	(°)	cut (J)	cut (J/cm <sup>2</sup> )	
1	27*27	27*27	5.20	1.92	Strains and	27*27	87	5.78	2.14	Rods and
2	27*27	27*27	5.49	2.03	leaves	27*27	85	6.07	2.25	leaves
3	27*27	27*27	5.49	2.03	leaves	27*27	86	5.92	2.19	leaves
4	27*27	27*27	5.78	2.14	Ctrains and	27*27	84	6.21	2.30	Dodo and
5	27*27	27*27	5.78	2.14	Strains and leaves	27*27	84	6.21	2.30	Rods and leaves
6	27*27	27*27	5.78	2.14	leaves	27*27	83	6.36	2.35	leaves
7	27*27	27*27	5.92	2.19	Ctusins and	27*27	82	6.50	2.41	Dada and
8	27*27	27*27	5.92	2.19	Strains and leaves	27*27	82	6.50	2.41	Rods and leaves
9	27*27	27*27	6.07	2.25	leaves	27*27	82	6.50	2.41	leaves
					Table 13					Table 14
Cı	utting the	fresh corn	stalk san	nples. Cuttii	ng angle	Cutting th	ne fresh c	orn stalk s	samples. C	cutting angle
	k	nife $0^{\circ}$ , sh	arpening	angle 20 <sup>0</sup>			knife 0°,	sharpenii	ng angle 2	<b>5</b> 0
N.L.	Test-bar	Angle	Energy	Specific		Test-bar	Angle	Energy	Specific	
Nr.	size	indicator	needed to	energy to cut	Observation	size	indicator	needed to	energy to	Observation
crt.	(mm/mm)	(°)	cut (J)	(J/cm <sup>2</sup> )		(mm/mm)	(°)	cut (J)	cut (J/cm <sup>2</sup> )	
1	27*27	109	2.64	0.98	Dada and	27*27	102	3.61	1.34	Dada and
2	27*27	108	2.77	1.03	Rods and leaves	27*27	101	3.77	1.39	Rods and leaves
3	27*27	108	2.77	1.03	leaves	27*27	101	3.77	1.39	leaves
4	27*27	106	3.05	1.13	Dodo and	27*27	99	4.04	1.50	Dodo and
5	27*27	105	3.19	1.18	Rods and	27*27	98	4.19	1.55	Rods and
6	27*27	105	3.19	1.18	leaves	27*27	99	4.04	1.50	leaves
7	27*27	101	3.76	1.39	Rods and	27*27	98	4.19	1.55	Rods and

8	27*27	100	3.90	1.44	leaves	27*27	97	4.33	1.60	leaves
0	27*27	99	4.04	1.50		27*27	97	4.33	1.60	

					Table 15					Table 16
С	utting the i	fresh corn	stalk san	nples. Cuttir	ng angle	Cutting th	ie fresh si	unflower s	samples. C	cutting angle
	kn	ife $0^{\circ}$ , ang	le of shar	pening 30°			knife $0^{0}$ ,	sharpenir	ng angle 2	$o^o$
Nr.	Test-bar	Angle	Energy	Specific		Test-bar	Angle	Energy	Specific	
crt.	size	indicator	needed to	energy to cut	Observation	size	indicator	needed to	energy to	Observation
G.	(mm/mm)	(°)	cut (J)	(J/cm <sup>2</sup> )		(mm/mm)	(°)	cut (J)	cut (J/cm <sup>2</sup> )	
1	27*27	101	3.76	1.39	Rods and	27*27	105	3.19	1.82	Especially
2	27*27	99	4.04	1.50	leaves	27*27	103	3.47	1.29	rods and
3	27*27	99	4.04	1.50	icaves	27*27	104	3.33	1.23	sloppy leaves
4	27*27	97	4.33	1.60	Rods and	27*27	100	3.90	1.44	Especially
5	27*27	96	4.47	1.66	leaves	27*27	100	3.90	1.44	rods and
6	27*27	96	4.47	1.66	leaves	27*27	99	4.04	1.50	sloppy leaves
7	27*27	93	4.90	1.82	Rods and	27*27	98	4.19	1.55	Especially
8	27*27	94	4.76	1.76	leaves	27*27	98	4.19	1.55	rods and
9	27*27	93	4.90	1.82	leaves	27*27	95	4.62	1.71	sloppy leaves
					Table 17					Table 18
	Cutting the fresh sunflower samples. Cutting angle									
C	utting the i	fresh sunf	lower san	nples. Cuttir	ng angle	Cutting to	he fresh s	unflower	samples. (	Cutting angle
C		fresh sunf nife 0º, sh			ng angle	Cutting to			samples. ( arpening 3	Cutting angle
		nife $0^{\circ}$ , sh			ng angle	Cutting to	knife 0°, a			Cutting angle
Nr.	k	nife 0º, sh Angle	arpening Energy	angle 25 <sup>0</sup>			knife 0°, a	Energy	arpening 3	Cutting angle
	<b>k</b> i Test-bar	nife $0^{\circ}$ , sh	arpening Energy	angle 25 <sup>0</sup> Specific		Test-bar	knife 0°, a	Energy	arpening 3 Specific	Cutting angle
Nr.	Test-bar size	nife 0º, sh Angle	Energy needed to	angle 25 <sup>0</sup> Specific energy to cut		Test-bar size	knife 0°, a	Energy needed to	arpening 3 Specific energy to	Cutting angle
Nr. crt.	Test-bar size (mm /mm)	Angle indicator(°)	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation	Test-bar size (mm /mm)	Angle indicator(°)	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Cutting angle $g^0$ Observation
Nr. crt.	Test-bar size (mm/mm) 27*27	Angle indicator(°)	Energy needed to cut (J) 4.33	Specific energy to cut (J/cm²)	Observation  Especially	Test-bar size (mm /mm) 27*27	Angle indicator(°)	Energy needed to cut (J) 4.90	Specific energy to cut (J/cm²)	Observation  Especially
Nr. crt.	Test-bar size (mm /mm) 27*27 27*27 27*27	Angle indicator(°)  97  95  96	Energy needed to cut (J) 4.33 4.62 4.47	Angle 25 <sup>0</sup> Specific energy to cut (J/cm <sup>2</sup> ) 1.60 1.71 1.66	Observation  Especially rods and	Test-bar size (mm /mm) 27*27 27*27 27*27	Angle indicator(°)  93  92  92	Energy needed to cut (J) 4.90 5.05	Specific energy to cut (J/cm²) 1.82 1.87	Observation  Especially rods and sloppy leaves
Nr. crt.	Test-bar size (mm /mm) 27*27 27*27	Angle indicator(°)  97  95	Energy needed to cut (J) 4.33 4.62	Specific energy to cut (J/cm²) 1.60 1.71	Observation  Especially rods and sloppy leaves Especially	Test-bar size (mm /mm) 27*27 27*27	Angle indicator(°)  93  92	Energy needed to cut (J) 4.90 5.05	Specific energy to cut (J/cm²) 1.82 1.87	Observation  Especially rods and sloppy leaves  Especially
Nr. crt.  1 2 3	Test-bar size (mm /mm) 27*27 27*27 27*27	Angle indicator(°)  97  95  96	Energy needed to cut (J) 4.33 4.62 4.47	Angle 25 <sup>0</sup> Specific energy to cut (J/cm <sup>2</sup> ) 1.60 1.71 1.66	Observation  Especially rods and sloppy leaves	Test-bar size (mm /mm) 27*27 27*27 27*27	Angle indicator(°)  93  92  92	Energy needed to cut (J) 4.90 5.05	Specific energy to cut (J/cm²) 1.82 1.87	Observation  Especially rods and sloppy leaves  Especially rods and
Nr. crt.  1 2 3	Ki Test-bar size (mm /mm) 27*27 27*27 27*27 27*27	Angle indicator(°)  97  95  96	Energy needed to cut (J) 4.33 4.62 4.47	Angle 25 <sup>0</sup> Specific energy to cut (J/cm²) 1.60 1.71 1.66	Observation  Especially rods and sloppy leaves Especially	Test-bar size (mm /mm) 27*27 27*27 27*27	Angle indicator(°)  93  92  92	Energy needed to cut (J) 4.90 5.05 5.05	Specific energy to cut (J/cm²) 1.82 1.87 2.03	Observation  Especially rods and sloppy leaves  Especially
Nr. crt.  1 2 3 4 5	Ka Test-bar size (mm /mm) 27*27 27*27 27*27 27*27	Angle indicator(°)  97  95  96  95  94	Energy needed to cut (J) 4.33 4.62 4.47 4.62 4.76	angle 25 <sup>0</sup> Specific energy to cut (J/cm²) 1.60 1.71 1.66 1.71 1.76	Observation  Especially rods and sloppy leaves  Especially rods and sloppy	Test-bar size (mm /mm) 27*27 27*27 27*27 27*27	Angle indicator(°)  93  92  92  89  88	Energy needed to cut (J) 4.90 5.05 5.05 5.49 5.63	specific energy to cut (J/cm²) 1.82 1.87 1.87 2.03 2.09	Observation  Especially rods and sloppy leaves  Especially rods and
Nr. crt.  1 2 3 4 5	Rest-bar size (mm /mm) 27*27 27*27 27*27 27*27 27*27 27*27	Angle indicator(°)  97  95  96  95  94  93	Energy needed to cut (J) 4.33 4.62 4.47 4.62 4.76 4.90	angle 25 <sup>0</sup> Specific energy to cut (J/cm²) 1.60 1.71 1.66 1.71 1.76 1.82	Observation  Especially rods and sloppy leaves  Especially rods and sloppy leaves	Test-bar size (mm /mm) 27*27 27*27 27*27 27*27 27*27	Angle indicator(°)  93  92  92  89  88  86	Energy needed to cut (J) 4.90 5.05 5.05 5.49 5.63 5.92	arpening 3 Specific energy to cut (J/cm²) 1.82 1.87 1.87 2.03 2.09 2.19	Observation  Especially rods and sloppy leaves  Especially rods and sloppy leaves
Nr. crt.  1 2 3 4 5 6	Rest-bar size (mm /mm) 27*27 27*27 27*27 27*27 27*27 27*27 27*27 27*27 27*27	Angle indicator(°)  97  95  96  95  94  93	Energy needed to cut (J) 4.33 4.62 4.47 4.62 4.76 4.90	Angle 25 <sup>0</sup> Specific energy to cut (J/cm²) 1.60 1.71 1.66 1.71 1.76 1.82	Observation  Especially rods and sloppy leaves  Especially rods and sloppy leaves  Especially rods and sloppy leaves  Especially	Test-bar size (mm /mm) 27*27 27*27 27*27 27*27 27*27 27*27 27*27 27*27 27*27	Angle indicator(°)  93  92  92  89  88  86	Energy needed to cut (J) 4.90 5.05 5.05 5.49 5.63 5.92 5.78	arpening 3 Specific energy to cut (J/cm²) 1.82 1.87 1.87 2.03 2.09 2.19	Observation  Especially rods and sloppy leaves  Especially rods and sloppy leaves  Especially rods and sloppy leaves  Especially

From the above, it appears that the best results in terms of energy consumption required for the cutting of the fibrous feed samples were made using the blades with a sharpening angle of  $20^{\circ}$ , and in cases where we increased the angle of sharpening at  $25^{\circ}$  and  $30^{\circ}$ , respectively, we had business with a significant increase in energy consumption when cutting samples.

Next, we retain the most convenient sharpening value obtained by the laboratory tests, the sharpen angle remains at 20°, and alter the tilting angle of the knife so as to achieve a truly sliding cutting process. In the same manner as before, we will proceed to the cutting of samples from fibrous feed materials, with the difference that the angle of inclination of the cutting knife changes, taking successive values of 20°, 25° or 30°. Applying the above, we obtain the following experimental values:

					Table 19					
Cu	Cutting the fresh lucerne samples. Knife with cutting angle 20°, sharpening angle 20°									
Nr. crt.	Test-bar size (mm /mm)	Angle indicator(°)	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation					
1	27*27	116	1.70	0.63	Tip of the					
2	27*27	114	1.96	0.73	stem with					
3	27*27	114	1.96	0.73	leaves					
4	27*27	110	2.50	0.93						
5	27*27	109	2.64	0.98	Rods and leaves					
6	27*27	104	3.33	1.23	104703					

				Table 20					
Cutting the fresh lucerne samples. Cutting angle knife 25°, sharpening angle 20°									
Test-bar size (mm /mm)	Angle indicator( <sup>0</sup> )	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation					
27*27	117	1.57	0.58	Tip of the					
27*27	116	1.70	0.63	stem with					
27*27	116	1.70	0.63	leaves					
27*27	111	2.36	0.87	5					
27*27	112	2.23	0.82	Rods and leaves					
27*27	110	2.50	0.93	100,400					

Table 22

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7	27*27	102	3.61	1.34	Rods at the
8	27*27	98	4.19	1.55	harvesting
9	27*27	97	4.33	1.60	level

27*27	109	2.64	0.98	Rods at the
27*27	107	2.91	1.08	harvesting
27*27	107	2.91	1.08	level

					Table 21
Cu			ne samples		h cutting
Nr. crt.	Test-bar size (mm /mm)	Angle indicator(°)	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation
1	27*27	119	1.31	0.49	Tip of the
2	27*27	118	1.44	0.53	stem with
3	27*27	116	1.70	0.63	leaves
4	27*27	115	1.83	0.68	Dadaaad
5	27*27	115	1.83	0.68	Rods and leaves
6	27*27	112	2.23	0.82	
7	27*27	111	2.36	0.87	Rods at
8	27*27	109	2.64	0.98	the harvesting
9	27*27	109	2.64	0.98	level

	the lucerne ting angle 2			
Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation
27*27 27*27	106 105	3.05	1.13	Tip of the stem with
27*27 27*27	103	3.47	1.29	leaves Rods and
27*27 27*27	99 99	3.61 4.04	1.34	leaves
27*27 27*27 27*27	98 99 98	4.19 4.04 4.19	1.55 1.50 1.55	Rods at the harvesting level

Cı	Table 23 Cutting the lucerne lucerne samples. Cutting angle knife 25°, sharpening angle 20°								
Nr. crt.	Test-bar size (mm /mm)	Angle indicator(0	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation				
1	27*27	108	2.77	1.03	Tip of the				
2	27*27	107	2.91	1.08	stem with				
3	27*27	106	3.05	1.13	leaves				
4	27*27	105	3.19	1.18					
5	27*27	103	3.47	1.29	Rods and leaves				
6	27*27	102	3.61	1.34	leaves				
7	27*27	100	3.90	1.44	Rods at				
8	27*27	98	4.19	1.55	the harvesting				
9	27*27	98	4.19	1.55	level				

Table 24 Cutting the lucerne lucerne samples. Knife with cutting angle 30°, sharpening angle 20°									
Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation					
27*27 27*27 27*27	110 110 108	2.50 2.50 2.77	0.93 0.93 1.03	Tip of the stem with leaves					
27*27 27*27	107 104	2.77	1.08	Rods and leaves					
27*27 27*27 27*27	104 102 99	3.33 3.61 4.04	1.23 1.34 1.50	Rods at the harvesting					
27*27	99	4.04	1.50	level					

					Table 25					
Cu		vheat strav			n cutting					
	angle 20 <sup>0</sup> , sharpening angle 20 <sup>0</sup>									
Nr. crt.	Test-bar size (mm /mm)	Angle indicator (°)	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation					
1	27*27	95	4.62	1.71						
2	27*27	94	4.76	1.76	Rods					
3	27*27	91	5.20	1.92						
4	27*27	92	5.05	1.87						
5	27*27	90	5.34	1.98	Rods					
6	27*27	88	5.63	2.09						
7	27*27	87	5.78	2.14						
8	27*27	87	5.78	2.14	Rods					
9	27*27	87	5.78	2.14						

Cutting	Table 26 Cutting the wheat straw samples. Cutting angle knife 25°, sharpening angle 20°										
Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation							
27*27	97	4.33	1.60								
27*27	97	4.33	1.60	Rods							
27*27	95	4.62	1.71								
27*27	94	4.76	1.76								
27*27	94	4.76	1.76	Rods							
27*27	93	4.90	1.82								
27*27	90	5.34	1.98								
27*27	91	5.20	1.92	Rods							
27*27	90	5.34	1.98								

					Table 27					Table 28
Cu	Cutting the wheat straw samples. Knife with cutting angle 30°, sharpening angle 20°								samples. Kr ening angle	
Nr. crt.	Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation	Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Obser- vation
1	27*27	99	4.04	1.50		27*27	110	2.50	0.93	Rods
2	27*27	98	4.19	1.55	Rods	27*27	109	2.63	0.98	and
3	27*27	97	4.33	1.60		27*27	108	2.77	1.03	leaves
4	27*27	97	4.33	1.60		27*27	108	2.77	1.03	Rods
5	27*27	94	4.76	1.76	Rods	27*27	105	3.19	1.18	and
6	27*27	94	4.76	1.76		27*27	102	3.61	1.34	leaves
7	27*27	93	4.90	1.82		27*27	100	3.90	1.44	Rods
8	27*27	92	5.05	1.87	Rods	27*27	99	4.04	1.50	and
9	27*27	92	5.05	1.87		27*27	97	4.33	1.60	leaves

Cı	Table 29 Cutting the fresh corn stalk samples. Cutting angle knife 25°, sharpening angle 20°							the fresh		•	Table 30 s. Knife with
Nr. crt.	Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation	_	Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation
1 2 3	27*27 27*27 27*27	111 110 109	2.36 2.50 2.63	0.87 0.93 0.98	Rods and leaves	-	27*27 27*27 27*27	116 114 114	1.70 1.96 1.96	0.63 0.73 0.73	Rods and leaves
4 5 6	27*27 27*27 27*27	109 107 106	2.63 2.91 3.05	0.98 1.08 1.13	Rods and leaves	-	27*27 27*27 27*27	112 111 107	2.23 2.36 2.91	0.82 0.87 1.08	Rods and leaves
7 8 9	27*27 27*27 27*27	103 100 99	3.47 3.90 4.04	1.29 1.44 1.50	Rods and leaves		27*27 27*27 27*27	105 101 100	3.19 3.76 3.90	1.18 1.39 1.44	Rods and leaves

					Table 31						Table 32
(	Cutting the										es. Cutting
	cutting angle 20°, sharpening angle 20°						а	ngle knife	25°, sharp	pening ang	gle 20 <sup>0</sup>
Nr.	Test-bar size	Angle	Energy needed	Specific energy			Test-bar size	Angle	Energy needed	Specific energy	
crt.	(mm /mm)	indicator (°)	to cut	to cut	Observation		(mm /mm)	indicator (°)	to cut	to cut	Observation
1	27*27	107	2.91	1.08	Especially	ŀ	27*27	110	2.50	0.93	Especially
2	27*27	105	3.19	1.18	rods and		27*27	108	2.77	1.03	rods and sloppy leaves
3	27*27	103	3.47	1.29	sloppy leaves		27*27	109	2.63	0.97	
4	27*27	101	3.76	1.39	Especially		27*27	106	3.05	1.13	Especially
5	27*27	100	3.90	1.44	rods and sloppy		27*27	105	3.19	1.18	rods and sloppy leaves
6	27*27	97	4.33	1.60	leaves		27*27	103	3.47	1.29	Sloppy leaves
7	27*27	97	4.33	1.60	Especially		27*27	102	3.61	1.34	Especially
8	27*27	95	4.62	1.71	rods and sloppy		27*27	99	4.04	1.50	rods and sloppy leaves
9	27*27	94	4.76	1.76	leaves		27*27	96	4.47	1.66	5.5pp) 100100

Table 34

Table 26

					Table 33	
(	Cutting the					
	cutting	g angle 20	$^{ ho}$ , sharpe	ning angle	e <b>20</b> º	
Nr. crt.	Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation	
1	27*27	112	2.23	0.82	Especially	
2	27*27	110	2.50	0.93	rods and sloppy	
3	27*27	109	2.63	0.98	leaves	
4	27*27	109	2.63	0.98	Especially	
5	27*27	106	3.05	1.13	rods and sloppy	
6	27*27	104	3.33	1.23	leaves	
7	27*27	101	3.76	1.39	Especially	
8	27*27	99	4.04	1.50	rods and	
9	27*27	99	4.04	1.50	sloppy leaves	

Cutting the fresh sunflower samples. Cutting angle knife 25°, sharpening angle 20°									
Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation					
27*27 27*27	104 103	3.33 3.47	1.23 1.29	Strains and					
27*27	102	3.61	1.34	leaves					
27*27	102	3.61	1.34						
27*27	99	4.04	1.50	Strains and leaves					
27*27	99	4.04	1.50	icaves					
27*27	98	4.19	1.55						
27*27	97	4.33	1.60	Strains and leaves					
27*27	95	4.62	1.71	icaves					

Table 3 Cutting the Iolium samples. Cutting angle knife 25°,										
	sharpening angle 20°									
Nr. crt.	Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation					
1	27*27	107	2.91	1.08	Strains and					
2	27*27	105	3.19	1.18	leaves					
3	27*27	105	3.19	1.18	icaves					
4	27*27	104	3.33	1.23	Strains and					
5	27*27	103	3.47	1.29	leaves					
6	27*27	100	3.90	1.44	leaves					
7	27*27	100	3.90	1.44						
8	27*27	99	4.04	1.50	Strains and leaves					
9	27*27	98	4.19	1.55	icaves					

	rabie 36								
Cutting the lolium samples. Knife with cutting angle 30°, sharpening angle 20°									
Test-bar size (mm /mm)	Angle indicator	Energy needed to cut (J)	Specific energy to cut (J/cm²)	Observation					
27*27	109	2.64	0.98	Strains and leaves					
27*27	109	2.64	0.98						
27*27	107	2.91	1.08						
27*27	106	3.05	1.13	Strains and leaves					
27*27	105	3.19	1.18						
27*27	103	3.47	1.29						
27*27	103	3.47	1.29	Strains and leaves					
27*27	101	3.76	1.39						
27*27	100	3.90	1.44						

After a simple analysis, it can be noticed that the specific cutting energy values vary not only depending on the humidity or origin and type of the feed material samples used during the experimental laboratory determinations, but also according to the place where the cutting along the rod the knife sharpening angle, and the degree of inclination of the knife used for cutting, as well as a number of other factors that are not considered in this research phase.

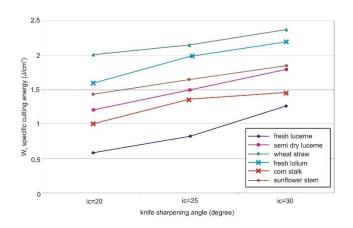
There is a decrease, in some cases even significant, of the value of the specific cutting energy, starting from the base of the stem, to the tip of the stem. This is represented in the graphs below, grouping the values of the specific cutting energy into three value groups, while taking into account the constructive angles of the knife.

The first group is the specific energy values for cutting in the upper area of the feed material rods used as test samples, where the rods are mostly thin, with many leaves, the relative humidity of this part is higher and, last but not least, the rods contain tissues young, soft. In this first group, we can analyze a constructive variant, which is the straight knife variant, where only the angle of sharpening  $i_c$  changes, but the angle of inclination of the alpha knife is equal to zero;  $\alpha = 0$ . Under these conditions, we obtain according to Figure 3. a slow increase in the specific cutting energy values due to the gradual increase in sharpen angle values. In fact, this phenomenon occurs when using uncut knives, blunted due to a high workload. There is also a well-known phenomenon, namely the increase of the specific energy in the cutting of fodder materials with a low humidity, such as the grinding of wheat straw, where the humidity determined during the laboratory experiments did not exceed 6%.

At high relative humidity levels of plants, in the case of semy dry lucerne or corn and sunflower, the cutting-specific energy gets lower values, cuts can be made easier, and hence a number of functional exploitation advantages, lower costs accounted for per kg of harvested forage.

We must also remember that it is very important to choose the material from which the knife is made. Good materials, quality steels are more expensive but resist over time, keep the angle of sharpening longer, their wear is reduced. Poor quality steels cost less, but their use is limited precisely because of repeated regrinding and their premature exit from use (*Caba I. 2006*).

These losses also have to be added to the losses suffered by the company through the non-use, the stagnation of the machinery, mostly due to the increased working capacity with these knives.



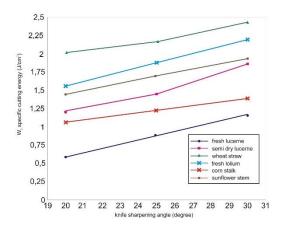


Fig. 3 - Variation of the specific cutting energy according to the angle of the knife sharpening. The samples contain leaves and rods at the top

Fig. 4 - Variation of the specific cutting energy processed according to the angle of the knife sharpening. The samples contain leaves and rods at the top

Processing the experimental data represented graphically in Figure 3. obtained in laboratory conditions, using the statistics applied in mathematics, we traced the real curves, obtaining some straight lines related to the cuts made on the fodder samples made from different feeds, according to the legend of the Figure 4, with strictly linear variations, has confirmed the initial assumption, that is, the increase in the sharpness values of the cutting-chopping knife, entails increasing the values of the specific energies at cutting, resulting in extreme cases at forces so large that no cutting actually takes place, breaking the samples material, or even stopping the knife in the material of the test specimen used.

The second group, represented by Figure 5, signifies the specific cutting energy values from the middle of the length of the samples, the area where the fiber feed samples has, besides many rods and leaves, in most cases this ratio is substantially equal.

There is a noticeable increase in the specific energy required to cut samples from feed materials to the values recorded at the cutting of samples formed from foliage and stems at the tip of the plants.

This increase is due to the decrease of the foliage and the increase in the number of rods, which have a more pronounced lignin structure in this area of plants. The increase in specific cutting energy expressed as a percentage represents approximately 10-15%, copying the percentage increase expressed as a sharp increase in the knife sharpening angle.

Applying identically, as in the previous case, the statistical processing of the experimental values obtained in the laboratory determinations on fodder samples and graphs, a linear variation, represented in Figure 6 was also obtained. And in the third group, represented by Figure 7. the values of the specific cutting energy in the lower area of the plants near the harvest area, which have been used as cutting material, are found.

This area is rich in lignite, aging, and low-moisture tissue, with a marked lack of leaves. Rods are ubiquitous in this type of samples, the cross section of the stems is much higher compared to the cross section of the stems at the tips, they are characterized by the high resistance to penetration of the knife blade.

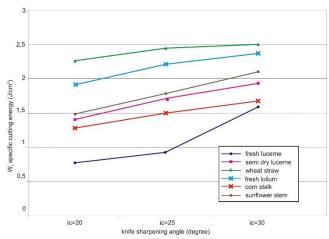


Fig. 5 - The specific cutting energy variation according to the angle of the knife sharpening.

The samples contain leaves and rods at the top

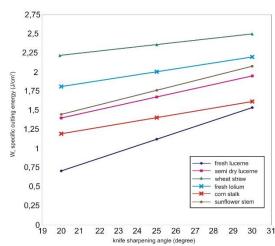


Fig. 6 - The specific cutting energy variation processed statisticaly according to angle of the knife sharpening. The samples contain leaves and rods at the top

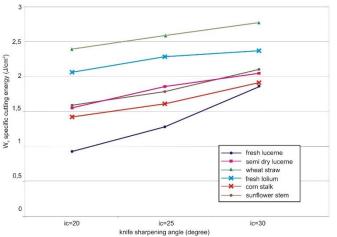


Fig. 7 - The specific cutting energy variation according to the angle of the knife sharpening. The samples contain leaves and rods at the top

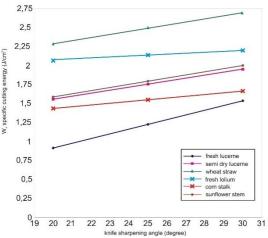


Fig. 8 - The specific cutting energy variation processed according to the angle of the knife sharpening.

The samples contain leaves and rods at the top

After the statistical processing of the values obtained in the laboratory tests at the cutting of samples from feed materials, we obtain, according to expectations, also a linear variation, but with higher values than in the other two studied cases, phenomenon explained by taking into account the increased resistance of the strains aged, ligninous, with a relatively lower moisture content as compared to the stem tips.

The sharpening and tilting angles of the knife also play an important role in modifying the specific cutting energy values, their correct choice depending on the material of the samples, its moisture content and other factors, may lead to a a significant decrease in the specific energy consumed in the cutting of the feed material used to make the daily feed of livestock from zootechnical farms.

This also results from the laboratory determinations performed on feed specimen specimens, where we modified only the angle of inclination alpha of the knife, while keeping the most convenient angle of sharpening, determined by the experimental tests performed, being  $i_c = 20^{\circ}$ . The specimen in this case, it mostly contains leaves and thin rods from the tip of the forage plant, from which it can be concluded that the cutting is carried out with a lower energy effort, according to Figure 9, we have values that gradually decrease with increasing the angle of inclination of the knife.

This decrease is not very spectacular and cannot be achieved to extreme values because of some conditions of exploitation and design of the shape of the knife and its resistance to daily exploitation. An inclination of more than 30° of the cutting-grinding knife in the laboratory experiment has made it technically impossible for the knife to be executed and used with the projector.

29 30

After performing the statistical processing of the obtained experimental data, we can see that this time a linear variation of the specific cutting energies was obtained, according to Figure 10.

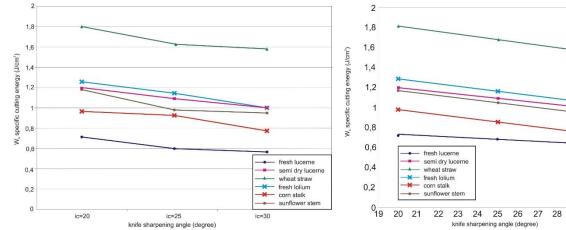


Fig. 9 - Specific energy variation when cutting the feed material samples from leaves and rods at the plant tip according to the angle of the knife sharpen at 20°

Fig. 10 - Specific energy variation processed statistically when cutting the feed material samples from leaves and rods at the plant tip according to the angle of the knife sharpen at 20°

If the angle of sharpening of the knife  $i_c = 20^{\circ}$  is maintained, but we vary the angle of inclination, using high-feed feed samples in rods and leaves harvested from the middle of the forage plants where the ratio of rods and leaves is substantially equal, values represented in Figure 11.

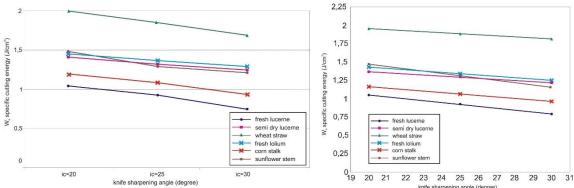


Fig. 11 - Specific energy variation when cutting the samples feed material with a rod content and leaves in the middle of the plant according to the inclination of the knife 20°

Fig. 12 - Specific energy variation processed statisticaly when cutting the samples feed material with a rod content and leaves in the middle of the plant according to the inclination of the knife 20<sup>0</sup>

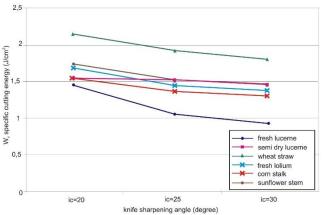


Fig. 13 - The specific energy variation when cutting the feed material specimen with a high rod content, depending on the inclination of the knife 20<sup>0</sup>

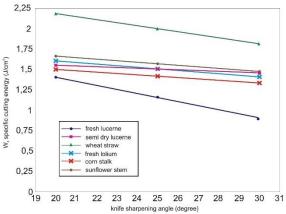


Fig. 14 - The specific energy variation processed statisticaly when cutting the feed material specimen with a high rod content, depending on the inclination of the knife 20°

As can be seen, a linear decrease in the specific energy required to perform the cutting of the samples was obtained in this case, which is shown in Figure 12.

The last evaluation of the specific cutting energy represented by Figure 13. which is carried out in the case of cuts made on samples of feed materials mainly made of rods with a high content of hard tissues, and in these determinations the value of the angle of sharpening the knife at  $i_c = 20^{\circ}$ , but altering the tilting of the knife, alpha, in those three previously known steps, previously described.

After the statistical processing of the experimental data obtained from the cutting of samples of feed materials with a high content of rods and this time a linear variation of the values of the specific cutting energies according to Figure 14 was obtained. There is a relative increase of these values compared to those obtained in the experiments performed on specimens with high leaf or mixed samples (leaves and rods) but after a realistic analysis it was found that this increase is justified by changing the structure of the stems, which are lighter, less water content, and last but not least we notice the total absence or low presence of leaves.

## **CONCLUSIONS**

Starting from the experimental results obtained from the laboratory research on the fibrous fodder organs, we obtained conclusive results which, after their processing, proved the veracity of the theory presented in the above chapters regarding the design of a cutting knife that is universally usable to the cutting-off of a variety of assortment of fibrous feed, irrespective of the maturity status or the time elapsed since harvesting.

In the first part of the experiments, straight knives were used and we only varied their angles of sharpening, from  $20^{\circ}$  to  $25^{\circ}$  or  $30^{\circ}$ , thus obtaining a permanent increase in the specific cutting energy (*Neculăiasa V., Dănilă I. 1995*). In the second part of the experiments carried out in the research laboratory, the angle of the most convenient knife sharpening angle of  $20^{\circ}$  was chosen, at which the specific cutting energy values were the lowest and we varied this time the angle of inclination of the knife  $20^{\circ}$ ,  $25^{\circ}$  and  $30^{\circ}$  to the corresponding cutting factor k = 0.36; k = 0.46 and k = 0.57.

Conclusions on the results obtained are as follows:

- 1) plant humidity significantly influences the consumption of the specific energy of cutting fodder plants;
- 2) specific cutting energy consumption varies according to the place where the cutting is done, higher at the base of the plants and gradually decreases towards the top of the plant:
- 3) the angle of sharpening of the knives has an important role in establishing the energy balance at the cutting-shredding of the plants, a small angle of sharpening leads to a specific consumption of low cutting energy, and if the angle of rotation increases, we have a significant increase in the specific energy of cutting;
- 4) sharpen angle of less than 20<sup>0</sup> leads to rapid knife cut, resulting in an increase in cutting-specific energy, knife rewind stops, machine productivity decreases, increases operating cost;
- 5) a solution to this problem is the use of knives made of special materials which do not require repeated re-drilling, but the cost of the special knives would be too high and their equally fragile, which would lead to their frequent change with repeated stops, the loss of precious harvest time;
- 6) the sharpening angle of more than 30<sup>0</sup> causes an excessive energy consumption of excessive cutting, especially in the case of drier fodders, because the actual cutting is partially replaced by the breaking of the fibrous feed material, vibrations occur during the cutting and even the clogging of the cutter;
- 7) a specific energy consumption of balanced cutting and at the same time a minimal wear of the blade cutting edge during the work we obtained at the angle of sharpening of the knife 25°, even with a material not recommended for making the knife;
- 8) while keeping the knife sharpening angle at 20<sup>0</sup>, where the specific cutting energy values were the smallest, we varied the tilting angle of the knife by which we obtained the sliding cut, the cutter energy values gradually decreasing with the increase of the inclination angle knife;
- 9) the highest cut-off energy values were recorded for the cutting angle 20° and the tilting angle of the knife 20° as well, and the lowest specific cutting energy values for the sharpen angle of 20° and the angle of inclination of the knife of 30°;
- 10) passing over these values causes some knife execution problems, and in extreme cases slipping the material on the cut.

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